

# Synthetic Near-Field Rock Motions in the New Madrid Seismic Zone

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## Participants

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Robert Hermann, Ph.D. (seismologist)



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## Outline of Presentation

- Objectives
- Overview of Study Area
- Characteristics of Near-Field Motions
- Generation of Synthetic Near-Field Rock Motions
- Discussion of Results
- Simulated vs. AASHTO & NCHRP 12-49 Spectra
- Comparison with other Simulation Methods
- Concluding Remarks



Rock Motions - 3



## Objectives

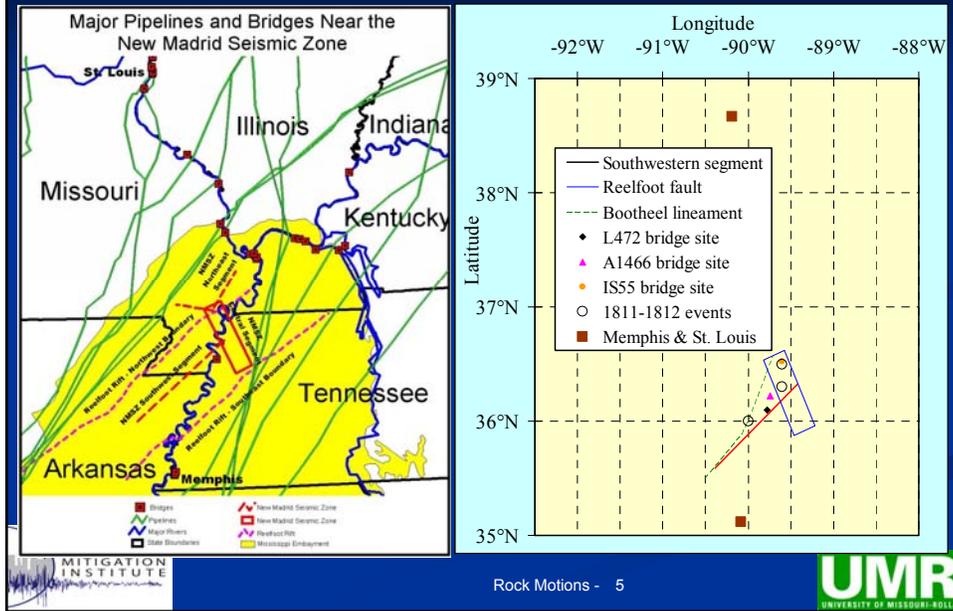
- To provide rock motion time histories at three bridge sites within the NMSZ for various combinations of moment magnitude and fault mechanism
- To evaluate near-field characteristics in the NMSZ
- To compare the spectra of the simulated motions with those of the AASHTO and the NCHRP 12-49 project
- To compare the results of the composite-source method with those of the finite-fault and the point-source models



Rock Motions - 4

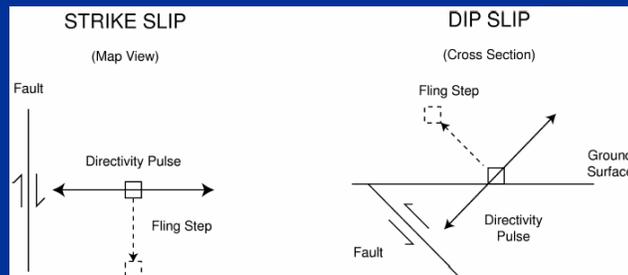


# Overview of Study Area



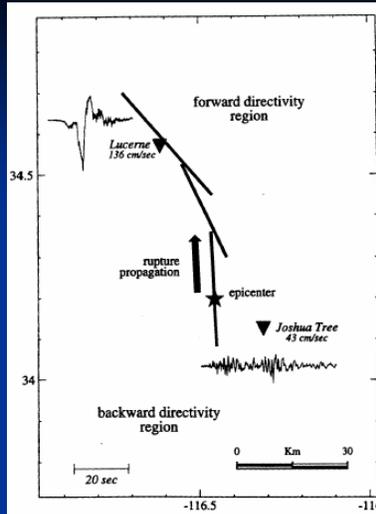
# Characteristics of Near-Field Motions

- **Forward Directivity:** rupture towards the site and is characterized by a two-sided velocity pulse(s) in the fault-normal direction
- **Fling Step:** characterized by one-sided velocity pulse in the same direction as the slip on the fault



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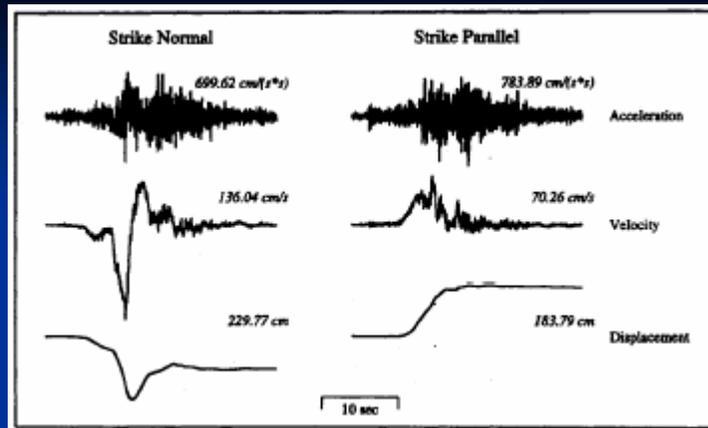




### 1992 Landers earthquake in Southern California (Strike-Slip Earthquake)



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### 1992 Landers earthquake - Lucerne Records

**Fault-normal:** *double-sided velocity pulse; small permanent displacement*

**Fault-parallel:** *single-sided velocity pulse; large permanent displacements*

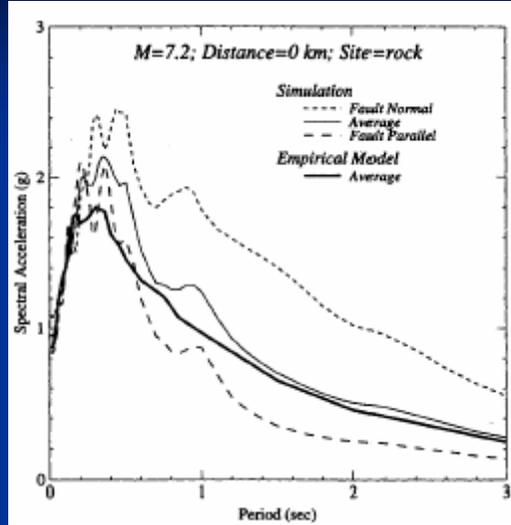


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## Effects of Forward Rupture Directivity

- Increase the amplitude of intermediate and long period ground motion
- Fault-normal component is larger than fault-parallel component at intermediate and long periods

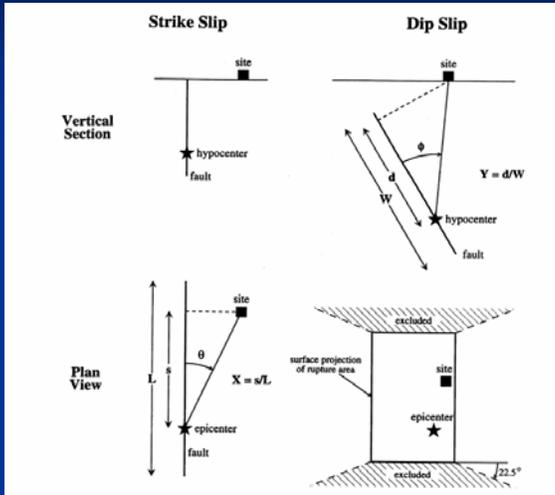
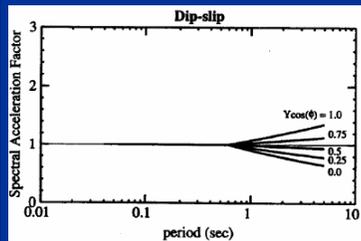
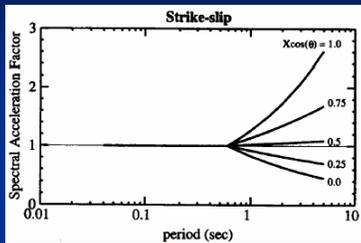


after Somerville et al. (1997)  
Rock Motions - 9



## Parameters of Forward Rupture Directivity

after Somerville et al. (1997)

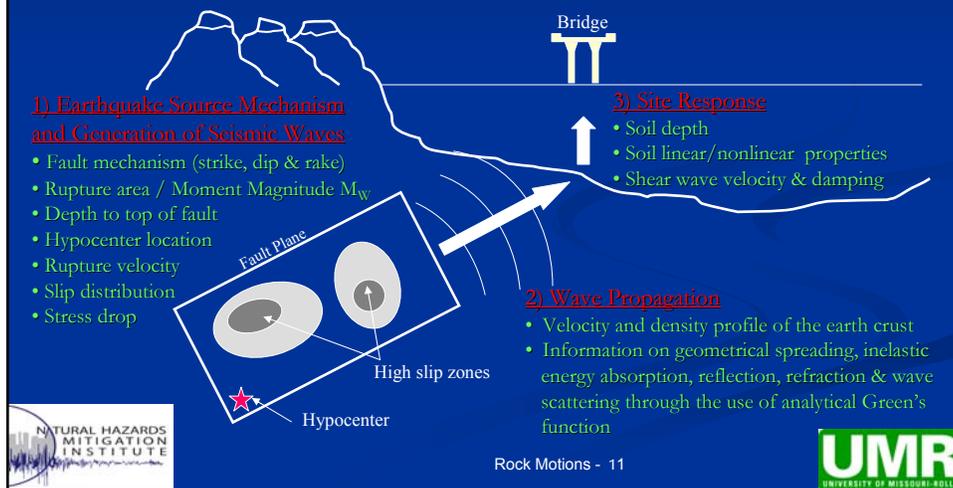


Directivity parameters:  $X \cos \theta$  for strike-slip faults  
 $Y \cos \Phi$  for dip-slip faults



# Generation of Synthetic Near-Field Ground Motions in the NMSZ

## *Earthquake Processes & Key Parameters*



## Seismic Source Parameters

*Best-estimates & uncertainties*

### Rupture Area

$$\log A = -3.42 + 0.90 M_w \quad s = 22\% (26\%)$$

*s is the standard deviation for strike-slip (reverse) faults after Wells & Coppersmith (1994)*

Fault	Best-estimate mechanism	Best-estimate rupture area
Southwestern segment (strike-slip fault)	Strike = 226.5° dip = 90° rake = 180°	L = 120 km, W = 18 km for $M_w$ 7.5,
		L = 56 km, W = 13.6 km for $M_w$ 7.0,
		L = 27 km, W = 10 km for $M_w$ 6.5
Reelfoot fault (reverse fault)	Strike = 156.1° dip = 32° rake = 90°	L = 82 km, W = 28 km for $M_w$ 7.5,
		L = 44 km, W = 18 km for $M_w$ 7.0,
		L = 22 km, W = 11 km for $M_w$ 6.5

## Seismic Source Parameters

*Best-estimates & uncertainties*

Depth to top of the fault

*1 km or 5 km*

Rake angle of slip on fault

*150, 180 or -150°*

Stress drop

*100, 150 or 200 bars*

Rupture velocity

*80% or 85% of  $V_S$*



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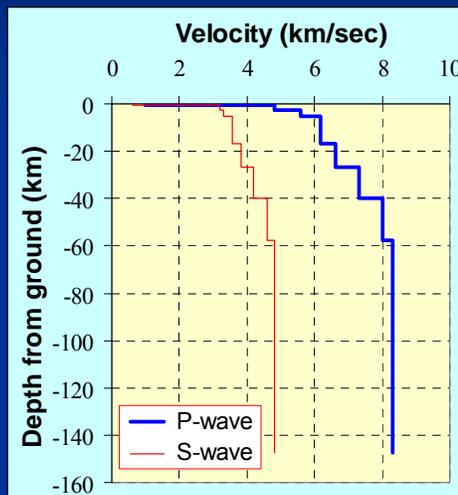
## Wave Propagation Parameters

*Best-estimates & uncertainties*

Velocity model  
of the earth crust

*Chiu et al. (1992)*

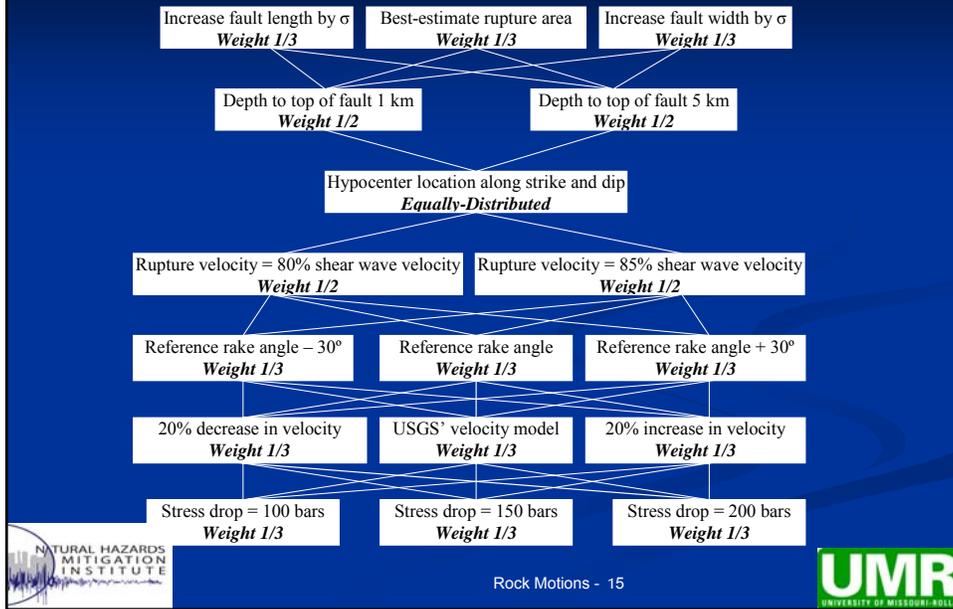
*20% variation*



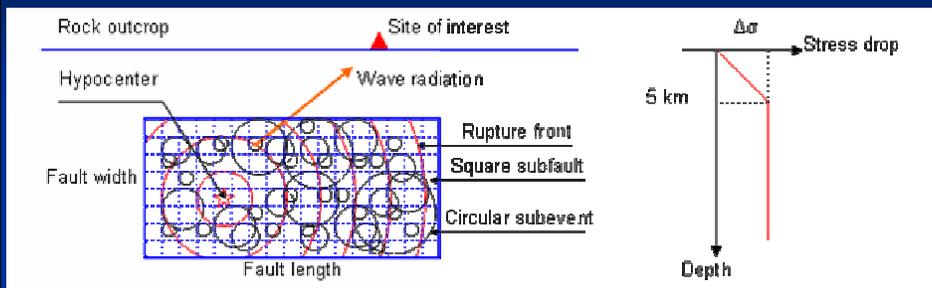
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# Logic Tree of Uncertain Parameters



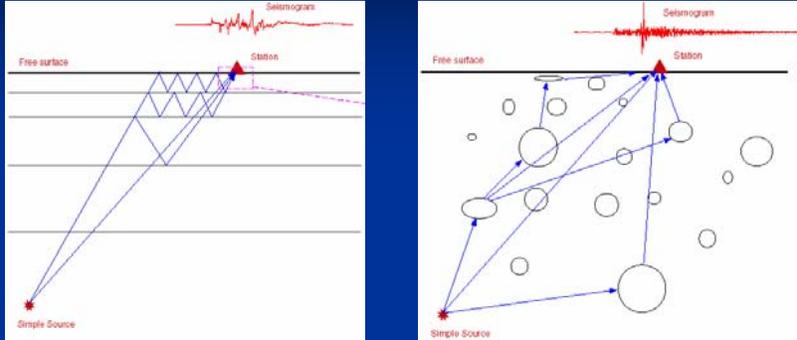
# The Composite Source Model



## Earthquake Source

The source of a strong earthquake is taken as a superposition of the radiation from a significant number of circular subevents with a constant stress drop. Rupture initiates at the presumed hypocenter and propagates radially at a constant rupture velocity. Each subevent is triggered when the rupture front reaches the center of the subevent. The subevent then initiates the radiation of a displacement pulse.

# The Composite Source Model



## Wave Propagation & Wave Scattering

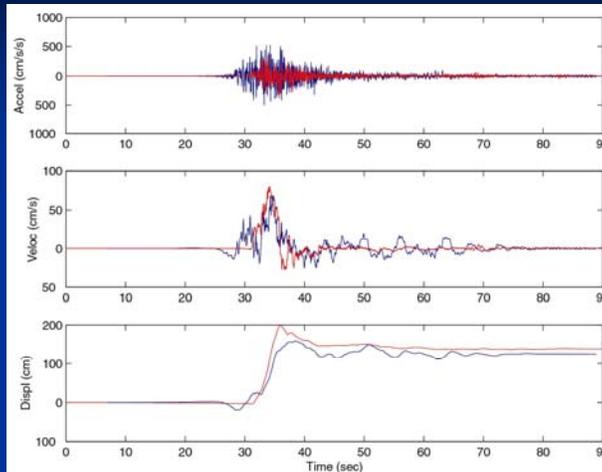
The generated displacement pulse propagates through a flat multi-layered earth crust. The wave propagation process is modeled with synthetic (analytical) Green's functions in both short- and long-period ranges. The short-period component is modified to account for the effects of random lateral heterogeneity of the earth by adding scattered waves.



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# The Composite Source Model Validation

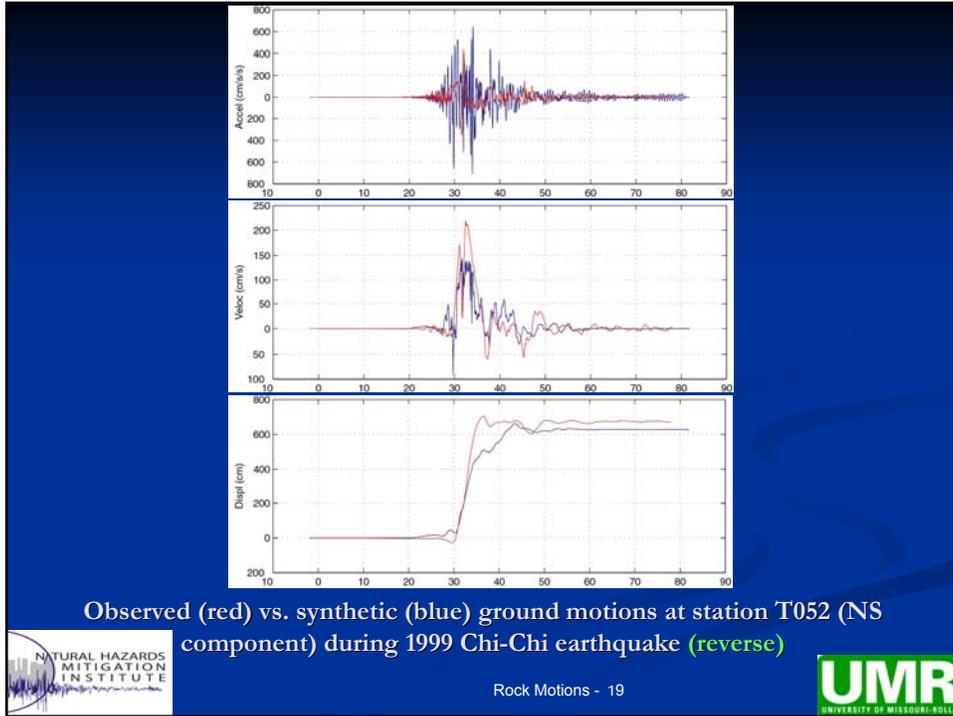


Observed (red) vs. synthetic (blue) ground motions at station SKR (east horizontal component) during 1999 Kocaeli earthquake (strike-slip)



Rock Motions - 18





## Discussion of Results of the Maximum Considered Earthquake (MCE) or $M_w$ 7.5

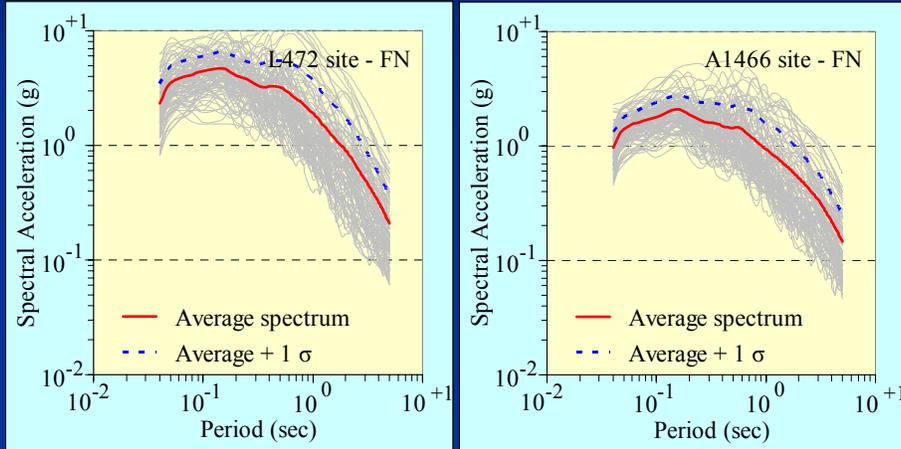
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# Total Uncertainty

## Southwestern segment

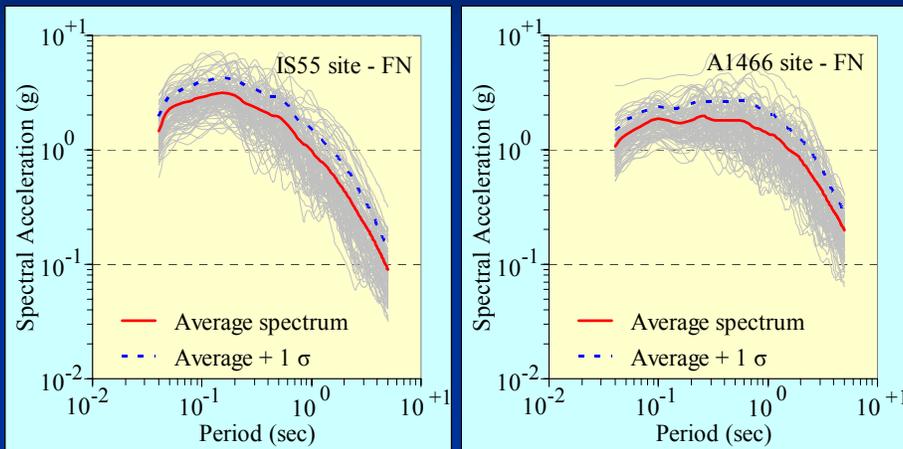


Rock Motions - 21



# Total Uncertainty

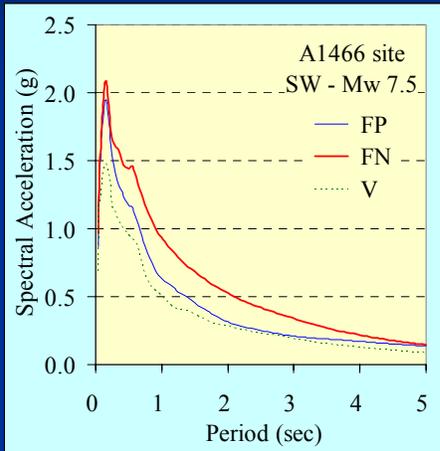
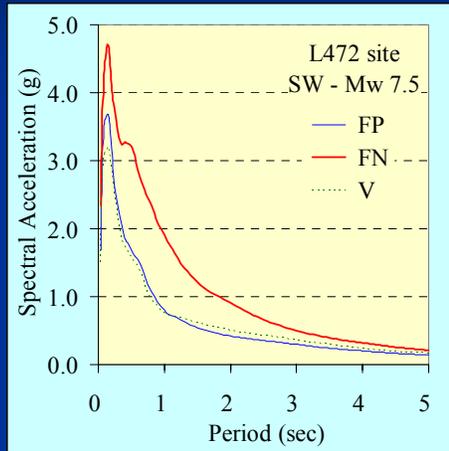
## Reelfoot fault



Rock Motions - 22



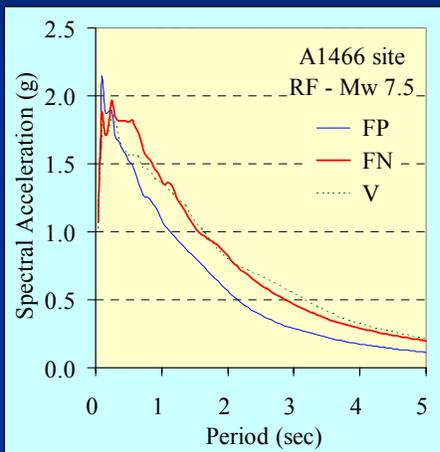
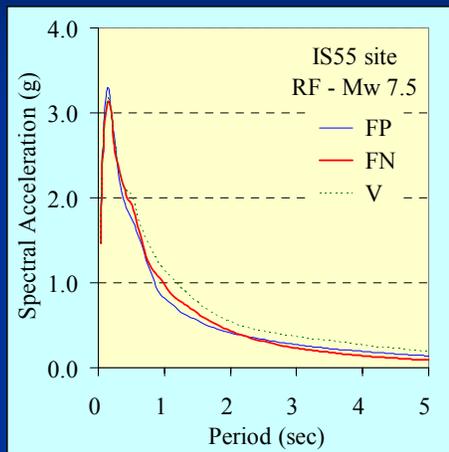
## Average Response Spectra Southwestern segment



Rock Motions - 23



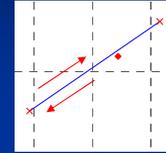
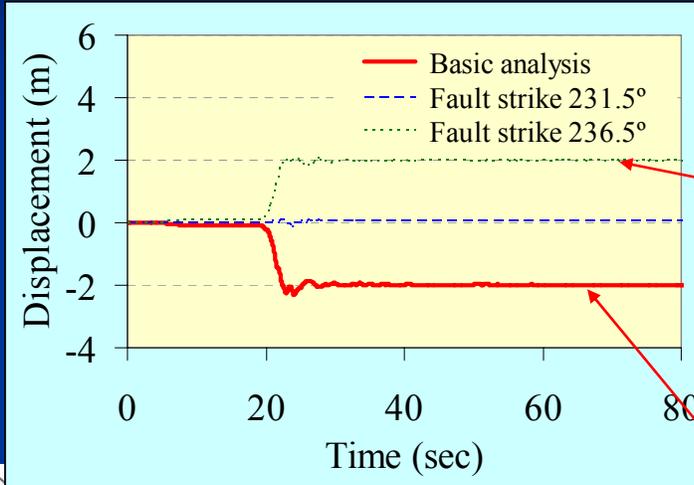
## Average Response Spectra Reelfoot fault



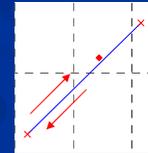
Rock Motions - 24



## Influence of Fault Mechanism on the Fling Step at L472 site



Fault strike 236.5°



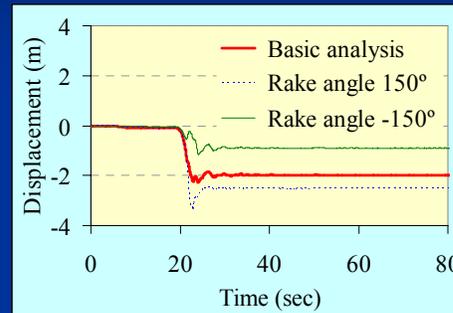
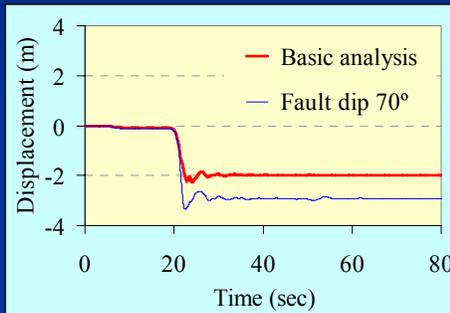
Fault strike 226.5°



Rock Motions - 25



## Influence of Fault Mechanism on the Fling Step at L472 site



For basic analysis:  
 Fault dip 90°  
 Rake angle 180°

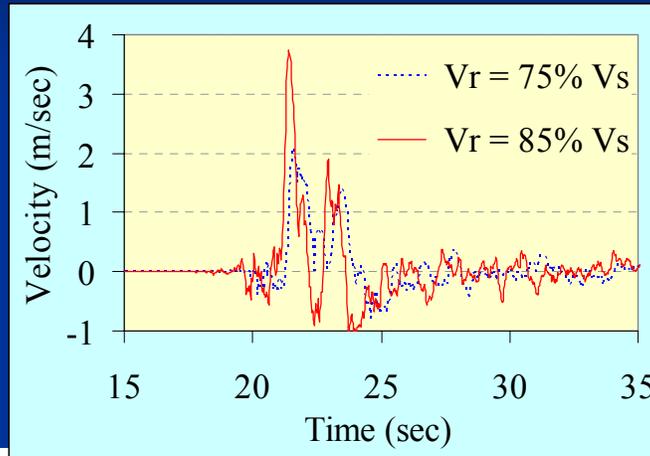


Rock Motions - 26





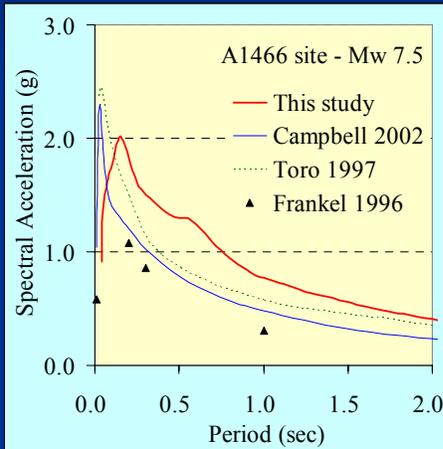
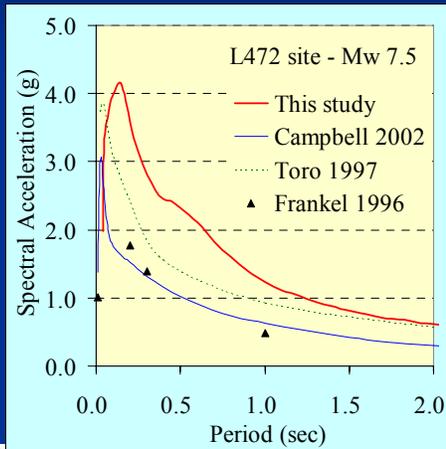
## Influence of Rupture Velocity on Velocity Pulses at L472 Site



Rock Motions - 29



## Validation of Synthetic Rock Motions Comparison with Attenuation Relations Southwestern segment

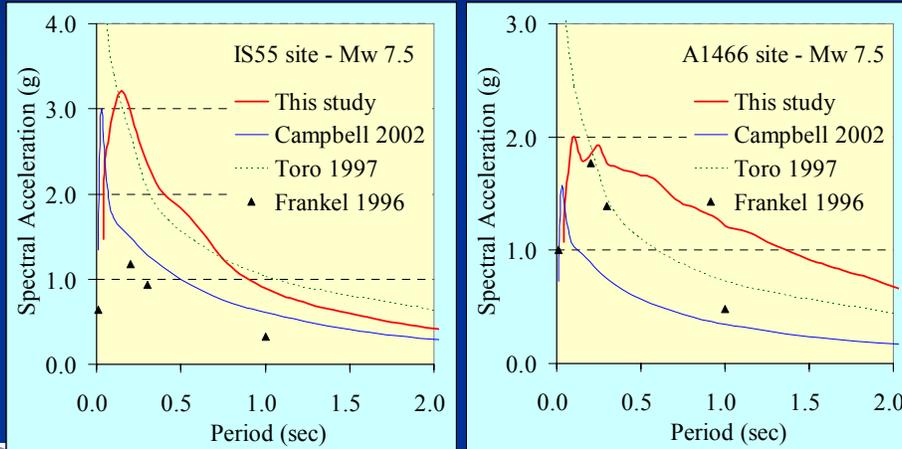


Rock Motions - 30



# Validation of Synthetic Rock Motions Comparison with Attenuation Relations

## Reelfoot fault

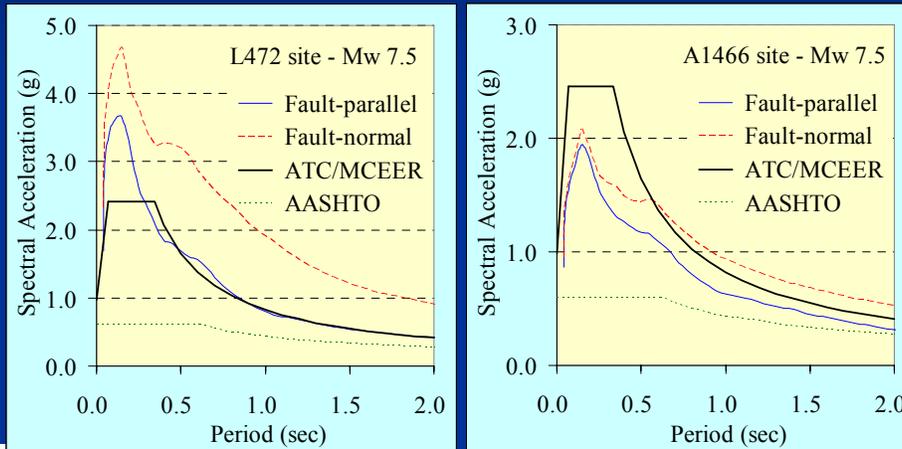


Rock Motions - 31



# Validation of Synthetic Rock Motions Comparison with NCHRP & AASHTO Guidelines

## Southwestern segment

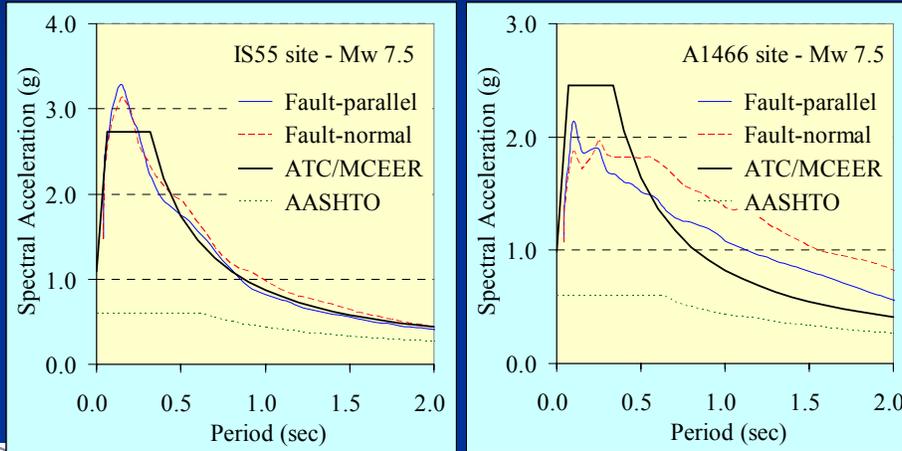


Rock Motions - 32



# Validation of Synthetic Rock Motions Comparison with NCHRP & AASHTO Guidelines

## Reelfoot fault

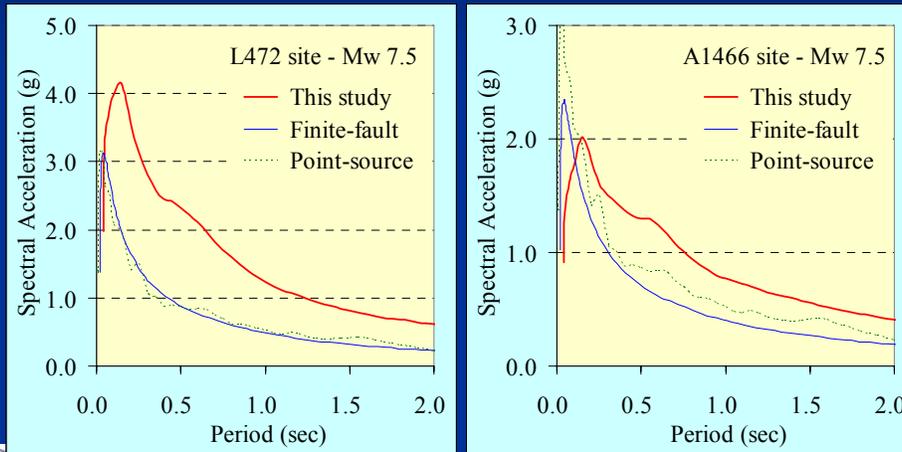


Rock Motions - 33



# Validation of Synthetic Rock Motions Comparison with Finite-Fault & Point-Source Models

## Southwestern segment

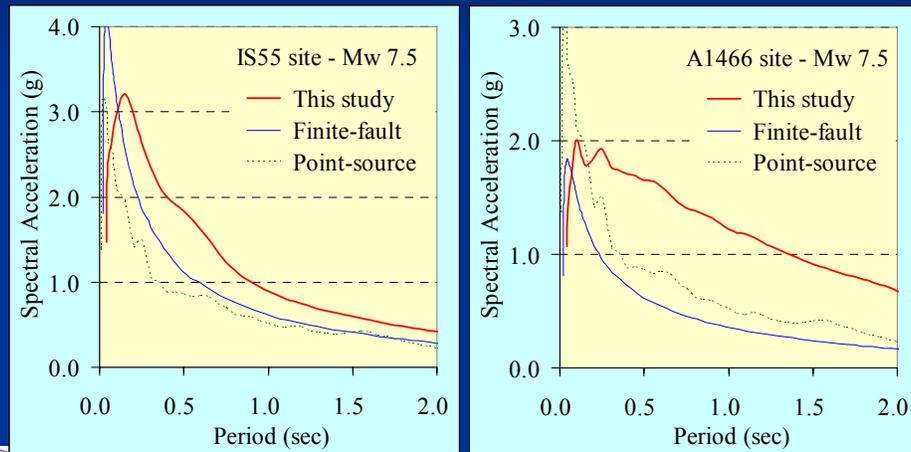


Rock Motions - 34



# Validation of Synthetic Rock Motions Comparison with Finite-Fault & Point-Source Models

## Reelfoot fault



Rock Motions - 35



## Near-Field Characteristics of the Selected Motions

### Selection criteria of rock motions

- 1) Fit the average response spectra
- 2) Fling step in the direction of the slip on the fault
- 3) Velocity pulse in the fault-normal direction
- 4) Realistic peak rock accelerations  
(within 75%-125% of Toro et al., 1997)

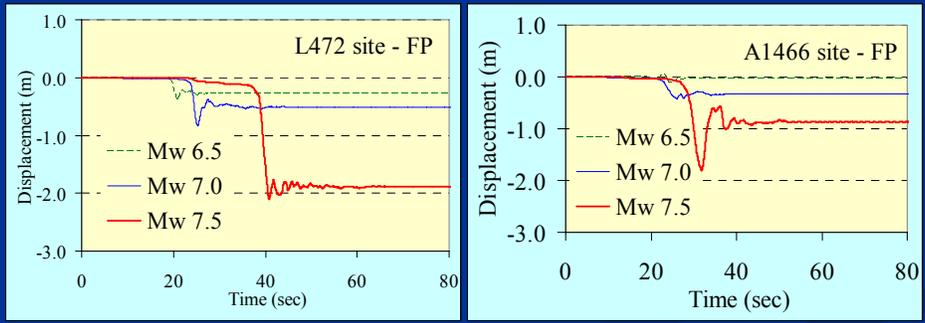


Rock Motions - 36



# Near-Field Characteristics of the Selected Motions

## Fling step from the southwestern segment

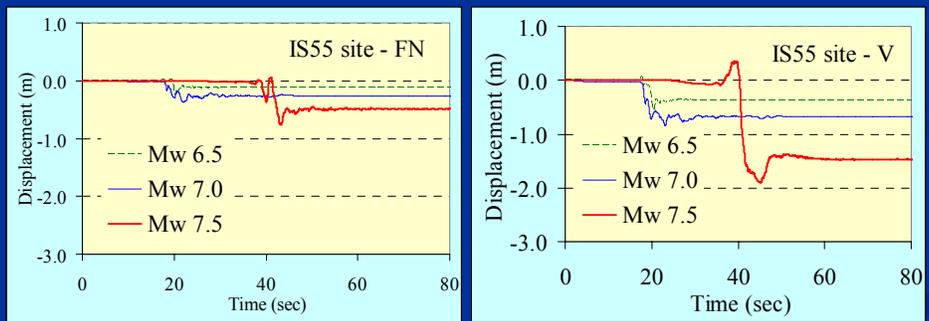


Rock Motions - 37



# Near-Field Characteristics of the Selected Motions

## Fling step from the Reelfoot fault

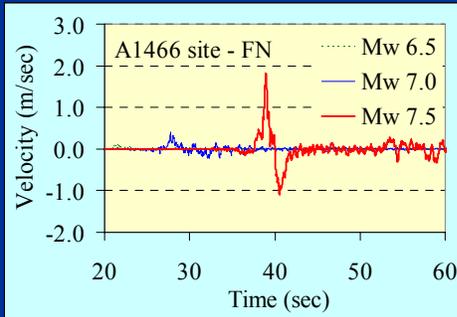
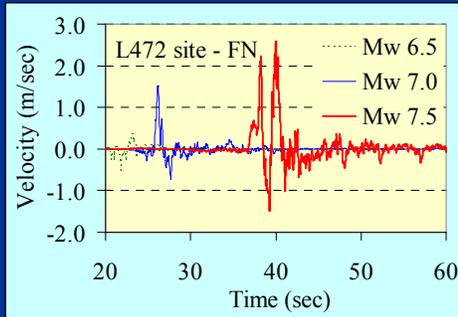


Rock Motions - 38



# Near-Field Characteristics of the Selected Motions

## Velocity pulse from the southwestern segment

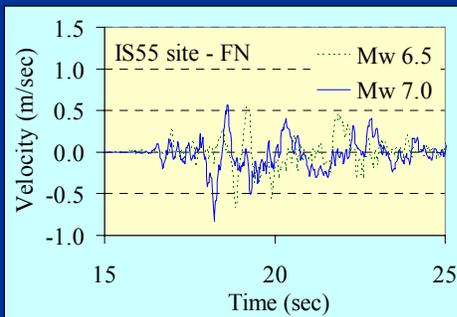
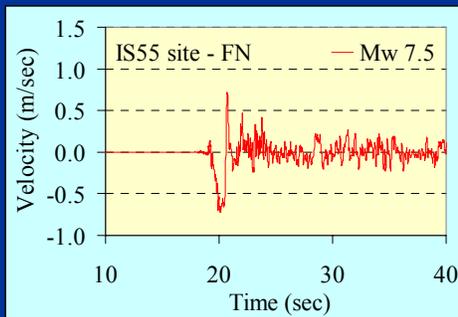


Rock Motions - 39



# Near-Field Characteristics of the Selected Motions

## Velocity pulse from the Reelfoot fault

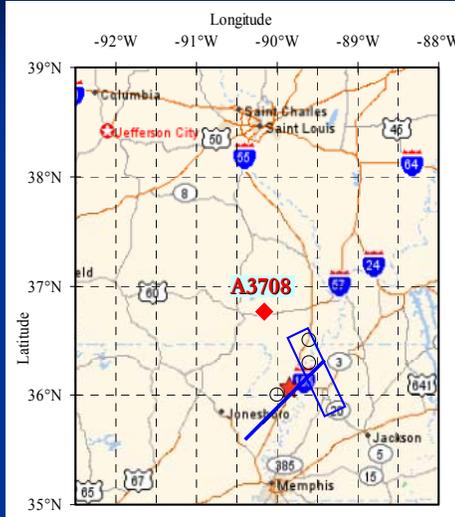


Rock Motions - 40



# St. Francis River Site (Far-Field)

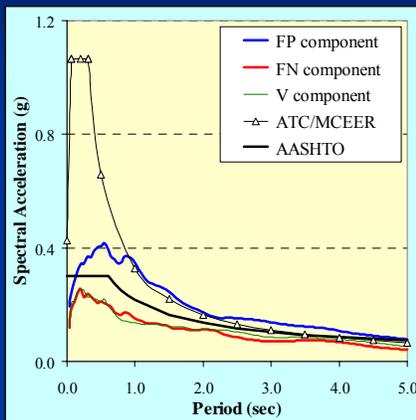
A3708 site is about 50km from the Reelfoot fault and 87km from the southwestern segment



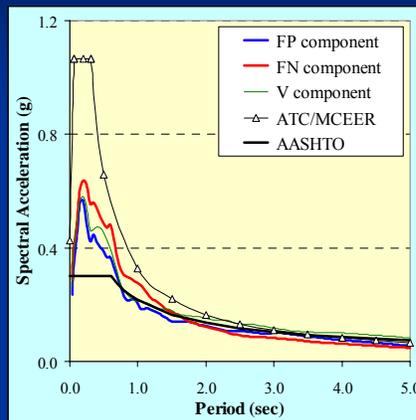
Rock Motions - 41



## Far-Field Rock Motions Comparison with NCHRP & AASHTO Guidelines



Southwestern segment



Reelfoot fault



Average of 20 simulations  
Rock Motions - 42



## Concluding Remarks

- The uncertainty of near-fault motions increases with moment magnitude and decreases with distance to fault
- The southwestern segment (strike-slip) contributes more to the total uncertainty than the Reelfoot fault (reverse) due to its forward rupture directivity effects
- The vertical component associated with the Reelfoot fault is stronger than that of the southwestern segment
- Fling step is dependent on the fault mechanism (strike, dip and rake), depth to top of the fault and stress drop



Rock Motions - 43



## Concluding Remarks

- Velocity pulses are dependent on the hypocenter location along the strike and rupture velocity
- The simulated spectral accelerations are higher than those of the attenuation relations, point-source or finite-fault models due to forward rupture directivity effects, particularly for  $M_w$  7.5 for strike-slip faults
- Velocity pulses associated with  $M_w$  7.5 are very large as compared to  $M_w$  7.0 or 6.5 that may impose special seismic demands for structures very close to active faults



Rock Motions - 44



## Concluding Remarks

- In comparison with ATC/MCEER spectra, the near-field motions in the proximity of the faults (<5 km) are generally higher, and those around 10km are similar in long period components but smaller in short period components.
- The far-field rock motion is on the average less than what ATC/MCEER specified in their recommended guidelines.

